A Review of Radiant Barrier and Interior Radiation Control Coatings Research Including Laboratory and Field Experiments

Mario A Medina, Ph.D., P.E.
Member ASHRAE

ABSTRACT

Attic Radiant Barriers (RBs) and Interior Radiation Control Coatings (IRCCs) are proven technologies that significantly reduce the flow of radiant heat across attic spaces, which in turn lowers the heat flow across the ceilings of buildings, ultimately lowering space cooling and heating loads, which produces energy and cost savings. This paper provides a general description of RBs and IRCCs, including installation configurations, the physical principles that make them work, and the methods used to evaluate their thermal performance, including laboratory and field experiments. An extensive review of the literature is summarized, highlighting fundamental issues, such as, reduced ceiling heat flows, reduced space cooling and heating loads, and changes in attic temperatures produced by the installation of RBs and IRCCs in residential attics. Causes that affect RB and IRCCs performance, such as the influence of attic insulation level and climate, are presented. The experimental data indicate that, on average, RBs reduce summer ceiling heat flows by 23 to 45% depending on the insulation level, whereas winter ceiling heat flow reductions are about 40% of the summer values for the same insulation levels. Similarly, the data indicate that RBs reduce space cooling loads by approximately 6 to 20% and that space heating loads reductions are also about 40% of the space cooling load values for the same insulation levels. Data from laboratory controlled experiments indicate that IRCCs with an emittance of 0.25 or less would reduce the ceiling heat flows by an amount equivalent to 61% of the values produced by RBs. Simulated data indicate that IRCCs would reduce the summer heat flows across the ceiling by an average of 25% in the presence of R-19 insulation. Simulated results predict that IRCCs installed in attics of residential buildings would reduce the space cooling load by an average of 14% and the space heating load by an average of 4%, in both cases for attics with an insulation level of R-11, where the air handling ducts are placed in the attic

INTRODUCTION

The increased pressure for reducing energy use and for lowering the electrical peak demand that result from building operations have encouraged the use and sometimes the excessive use of insulation. Although building insulation has played an essential role in making buildings more energy efficient, the amount of insulation that can be added to an attic space is limited by the physical dimensions of the ceiling frame. For example, most ceiling frames allow anywhere between 4 to 16 in. (10.2 to 40.6 cm) of insulation (Carter 2010). Extra insulation could potentially obstruct the attic ventilation air, compress itself, and create an excessive weight on the ceiling structure.

Attic Radiant Barriers (RBs) Interior Radiation Control Coatings (IRCCs) present a different way of increasing the thermal performance of existing or to-be-installed insulation within the space between roofs and ceilings of buildings (e.g., attic spaces in residential buildings or the space between roofs and suspended ceilings in commercial buildings) and have received considerable attention because of their potential to reduce the radiant heat transfer across vented spaces between roofs and ceilings of buildings. Radiant barriers are aluminum foil laminates or aluminized synthetic films sheets. The foils

Mario A Medina is an associate professor in the Department of Civil, Environmental, and Architectural Engineering, University of Kansas, Lawrence, Kansas.

are laminated to paper, most commonly to Kraft paper, synthetic films, to oriented strand board (OSB), or plywood. These laminates and films are characterized by having at least one low emittance surface of 0.1 or less (ASTM C 1313 2010). In the case of RBs, aluminum is used because it is inexpensive and because its surface, once exposed to air, becomes covered with a layer of a transparent oxide that protects it from the atmosphere and allows it to maintain a constant emittance for long periods of time (Lenntech 2010).

RBs are commonly installed in one of four configurations. These configurations are shown in Figure 1.

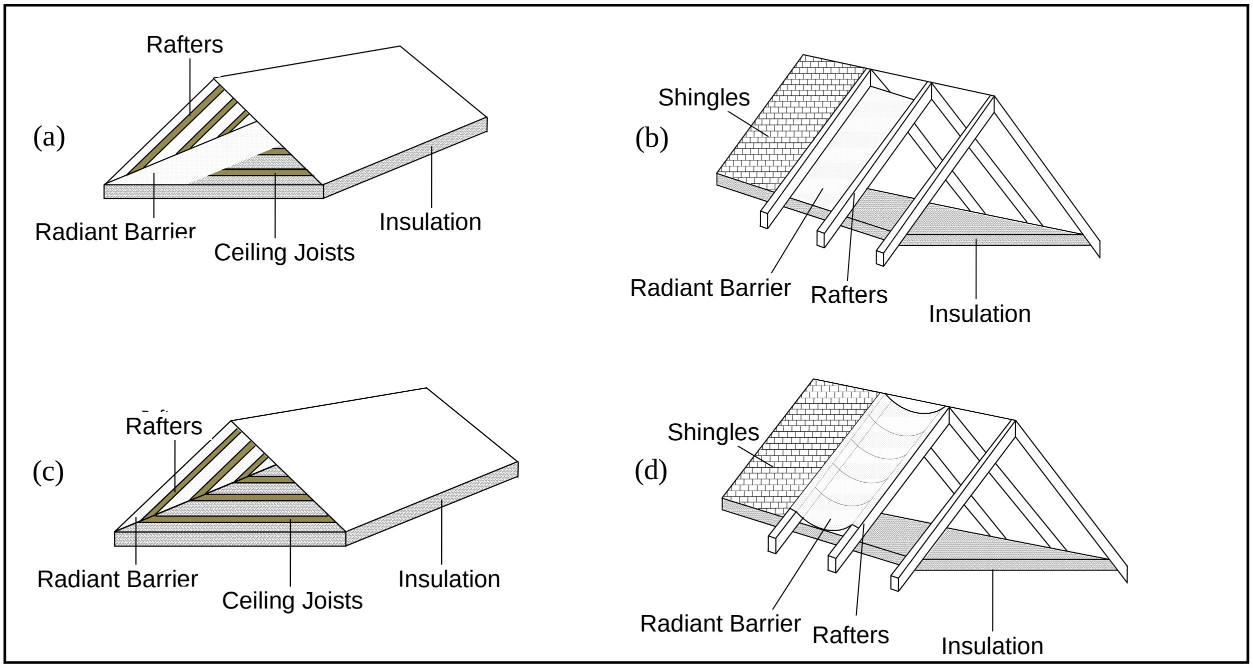

Figure 1. *Common radiant barrier installation configurations: (a) horizontal radiant barrier (HRB), (b) truss radiant barrier (TRB), (c) deck-applied radiant barrier (DARB), (d) draped radiant barrier (DRB).*

In the horizontal radiant barrier (HRB) configuration, the radiant barrier is installed on top of the ceiling insulation. In this case, if the radiant barrier has only one low emittance side, this side faces up towards the air space. The truss radiant barrier (TRB), consists of a radiant barrier installed within the trusses of the attic against the rafters that support the roof deck. In this configuration an extra air space is formed between the radiant barrier and the roof deck. If the radiant barrier has only one low emittance side, it is recommended that the low emittance side face the attic air space. The deck-applied radiant barrier (DARB) consists of aluminum foil bonded to the oriented strand board (OSB) or plywood boards that make up the roof deck. In the draped radiant barrier (DRB), the radiant barrier is attached to the roof deck or held between the roof deck and the rafters where the barrier is allowed to form a "drape-like" configuration, which in turn forms a narrow air space between the deck and the radiant barrier.

Interior Radiation Control Coatings (IRCCs) are not considered radiant barriers; however, they are similar in relation to the physical principles involved in decreasing the radiant heat flows across vented attic spaces. IRCCs are low emittance coatings or paints that when applied (i.e., sprayed or painted) to a building surface (e.g., OSB, plywood, metal siding, or plasterboard) the emittance of these surfaces changes to that of the coating, which is 0.25 or less (ASTM C 1321 2009). For most part, the configuration for the installation of IRCCs is similar to that of the deck-applied radiant barrier, Fig. 1(c), depending on whether or not the rafters are coated.

Because of their low emittance values RBs (ε = 0.1 or less) and IRCCs (ε = 0.25 or less) installed in attic spaces reduce the thermal radiation that is transferred between the roof deck and the top of the insulation, which is usually installed on the floor of the attic as shown in Figures 1(a) through 1(d). This reduction in radiation heat transfer can be partly explained by

Equation (1), which represents the net transfer of heat by radiation between two surfaces (e.g., roof deck, surface 1, and top of the insulation, surface 2)

$$\dot{q}_{12} = \frac{\sigma(T_1^4 - T_2^4)}{\frac{1 - \varepsilon_1}{A_1\varepsilon_1} + \frac{1}{A_1F_{12}} + \frac{1 - \varepsilon_2}{A_2\varepsilon_2}} \quad (1)$$

Basically, RBs and IRCCs work by altering the emittance value (ε) of at least one of the surfaces between the roof deck and top of the insulation, these included. Note that Equation (1) is an oversimplification in many ways, but it presents a snapshot of the physics involved when RBs or IRCCs are installed in attic spaces. For the TRB and DRP configurations other terms must be added to the denominator of Equation (1) because extra air spaces are created when the radiant barriers are installed.

Table 1. Comparisons of Radiant Heat Transfer Rates from a Hot Deck to the Top of the Insulated Ceiling Frame for Various RB and IRCC Configurations (T_{deck} = 130 °F, $T_{top\ of\ insulation}$ = 110 °F)

Surface 1 Emissivity (0 - 1)	Surface 2 Emissivity (0 - 1)	Surface 3,1 Emissivity (0 - 1)	Surface 3,2 Emissivity (0 - 1)	Representative Case	Radiant Heat Transfer Rate (Btu/hr ft²)	Reduction with Respect to Base Case (%)
0.93	0.85	-	-	Base Case (Standard Attic)	21.4	-
0.93	0.05	-	-	Horizontal Radiant Barrier	1.33	93.8
0.93	0.85	0.90(1)	0.05	Truss Radiant Barrier (One Aluminum Side)	1.25	94.2
0.93	0.85	0.05	0.90(1)	Truss Radiant Barrier (One Aluminum Side)	1.25	94.2
0.93	0.85	0.05	0.05	Truss Radiant Barrier (Two Aluminum Sides)	0.66	96.9
0.127(2)	0.85	-	-	Deck Applied Radiant Barrier	3.32	82.9
0.93	0.85	0.90(1)	0.127(2)	Draped Radiant Barrier (One Aluminum Side)	2.88	86.5
0.93	0.85	0.127(2)	0.90(1)	Draped Radiant Barrier (One Aluminum Side)	2.88	86.5
0.93	0.85	0.05	0.127(2)	Draped Radiant Barrier (Two Aluminum Sides)	0.95	95.5
0.23	0.85	-	-	IRCCs	5.92	72.4
0.29(3)	0.85	-	-	IRCCs	7.38	65.5

(1) Based on the emissivity of Kraft paper (Cole Parmer, 2010), (2) Based on the weighted emissivity of aluminum (0.05) and wood rafters (0.87) for ratios of 90.6% for RB and 9.4% for wood rafters, (3) Based on the weighted emissivity of a typical IRCC (0.23) and wood rafters (0.87) for ratios of 90.6% for RB and 9.4% for wood rafters

RADIANT BARRIER and IRCC PERFORMANCE

There are three well-established and accepted methods that are used for evaluating the performance of RBs, and thus, IRCCs. These are laboratory tests, field studies, and computer simulations. Laboratory tests have the advantage that several parameters, such as roof temperature, "solar" intensity, "wind" speeds, and others can be controlled, which allows first order parameters, such as ceiling heat fluxes and attic temperatures, to be isolated and studied. Although laboratory tests are well received and are essential in the study of radiant barriers, they present some drawbacks. One of the shortcomings of laboratory tests is that outdoor (i.e., weather-like) conditions are not entirely reproduced in a laboratory setting. As a result, most laboratory experiments are carried out under steady-state conditions, which are not representative of the conditions in which buildings operate. Field studies tend to be more complex, but offer the advantage that buildings are studied under full weather conditions. These studies produce data that most accurately represent the conditions in which buildings operate. Field studies also have their own complications and limitations. Complications arise from the fact that under full weather conditions the climatic variables are virtually impossible manage. The most precise results from field studies are produced when side-by-side testing procedures are performed using identical (i.e., same footprint, construction, size, and orientation) unoccupied buildings. In addition to the buildings being identical in all respects, it is important that the buildings' thermal performance be identical or nearly identical prior to the installation of the radiant barriers. In side-by-side testing protocols, control (i.e., standard) and test (i.e., retrofit) buildings operate under the same weather conditions and direct comparisons are therefore possible. A third method used to evaluate the thermal performance of radiant barriers is computer simulation using mathematical models. Although the review of the literature performed for this paper found several computer simulations of buildings with installed radiant barriers, these are presented in a separate paper.

Most of the results, both experimental and computational, are given in terms of ceiling heat fluxes and space cooling and space heating load reductions in percentages. This is because comparisons are often made between buildings with and buildings without radiant barriers and IRCCs. Therefore, the effectiveness (i.e., the "thermal performance") of radiant barriers and IRCC’s is often an indication of the percent reductions that RBs and IRCCs produce when buildings with RBs and IRCCs and buildings without RBs and IRCCs are compared.

Review of Experimental Works

Over fifty years (1958-2010) of published papers from various sources were reviewed. The most relevant results are summarized in Tables 1 through 5. The results of Tables 1 through 4 are presented in terms of percent reductions. The results in Table 5 are presented in terms of temperature reductions, in ^{o}F. For clarity, all percent reductions and temperature data were rounded off to the nearest whole number. The tables were divided into cooling and heating season tables. For the cooling season, only data collected during June, July, and August were considered. Similarly, for the heating season, only data collected during December, January, and February were considered. Within each table the results were grouped by insulation level. For most part only insulation levels of R-11 (1.94 m^2-K/W), R-19 (3.35 m^2-K/W), and R-30 (5.28 m^2-K/W) were included. Within each table, the percent reductions were also depicted graphically using shaded horizontal clustered bars. This was used as a visual tool. Also, because the data were from experiments from such a diverse pool and were carried out in various geographical locations, climate conditions, attic ventilation arrangements, in occupied and unoccupied buildings, etc., as much information as possible is presented in each table entry. This information includes testing protocol (i.e., laboratory controlled, side-by-side, or pre-and-post), location (city and state), cooling and heating degree days (base 65^{o}F, 18.3^{o}C), climatic zone (see Figure 2 below), ventilation type (i.e., natural or forced ventilation and vent arrangement), whether or not the building was occupied during the testing period, and whether or not the air handlers and ducts were located in the attics. In addition, average values are presented for each data cluster. For testing protocols, laboratory controlled experiments were performed under steady-state conditions. Side-by-side experiments were carried out simultaneously in two or more houses in which one house was used as a control house while the other(s) was (were) retrofit with radiant barriers in one of the four RB installation configurations. Pre-and-post experiments were carried out using the same buildings at different times, but under comparable weather conditions. That is, data were gathered first with the attic without radiant barriers. Subsequently, radiant barriers were installed and the monitoring continued. The cooling and heating degree days, as well as DOE climatic zones, for the experimental locations were provided to give a sense of the climate under which the experiments were carried out. All radiant barriers and IRCCs used in the experiments were new, clean radiant barriers and IRCCs.

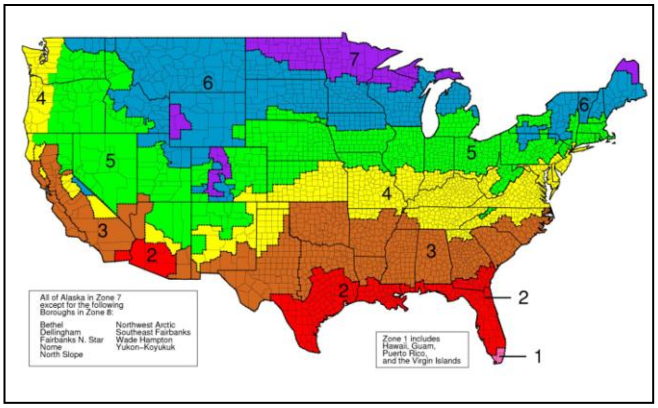

Figure 2. *U.S. climate zone map (ASHRAE Standard 169-2006, 2006)*

Table 1 shows the results of ceiling heat flow reductions produced by RBs and IRCCs during the cooling season. Laboratory-controlled experiments indicated that radiant barriers installed in flat roof systems provided higher percent reductions than those installed in pitched roofs. In both cases, the radiant barriers were installed in HRB configurations. Laboratory-controlled experiments of IRCC applied in flat roof configurations, with R-19 (3.35 m^2-K/W) insulation, produced average heat flow reduction of 32% (vs. the same system without the application of any coatings). In field experiments, radiant barriers installed in attics with R-11 (1.94 m^2-K/W) insulation produced ceiling heat flow reductions that ranged from 34% to 60%. The 60% corresponded to an attic in which both a HRB and a TRB were installed at the same time. That is, the attic interior was fully lined with a radiant barrier. The average reduction in heat flow produced by radiant barriers in attics with R-11 (1.94 m^2-K/W) insulation was 45%. In attics with insulation levels of R-19 (3.35 m^2-K/W) the reductions ranged from 16% to 43%, with an average value of 30%. The average reduction from installed HRBs was 29%. For installed TRBs the average reduction was 32%. Radiant barriers installed in the draped configuration (DRB) yielded an average of 18% reduction. There seemed to be a small correlation between percent reductions in ceiling heat flows and the geographical location of the buildings for the referenced experiments, most of which were carried out in DOE's Climatic Zones 2 and 4. For example, for the attics with installed HRBs, the highest percentages were observed in Zone 4 (as opposed to Zone 2), but for those attics with installed TRBs and DRBs the maximum reductions were observed in Zone 2 (as opposed to Zone 4). There also seemed to be a degree of correlation between the ceiling heat flow reductions and attic airflow patterns (e.g., soffit/soffit, soffit/gable, and soffit/ridge). For example, the houses that were identified as having a soffit vent for attic air intake and also a soffit vent for attic air exhaust had the largest percent reduction in ceiling heat flows when TRBs were installed. However, there was no clear correlation in percent reductions produced by TRBs in those houses with soffit/ridge or soffit/gable vents arrangements. There were also no clear correlations in ceiling heat flow reduction and attic airflow rate or with whether the airflows were naturally or forced across the attic. The only exception was from a study by Parker and Sherwin (1998) in which the heat flow percent reduction produced by a TRB increased 10 percentage points, from 26% to 36%, when the vent area for natural attic airflow was increased from 1:300 to 1:150. For attics with R-30 (5.28 m^2-K/W) insulation the reductions ranged between 20% and 25%, with an average value of 23%. These experiments indicated that for TRBs, the highest percent reductions were produced in Zone 2 (as opposed to Zone 4)

Table 1. Experimental Ceiling Heat Flow Reductions Produced by the RBs and IRCCs (Cooling Season)

Season	Reference	Nominal Insulation Level R-Value	Testing Protocol	Method	Ceiling Heat Flow Reductions Over Test Period (%) Summer														City, St	CDD	Climatic Zone	Ventilation				Occupied		Comments	Average
					-5	0 - 4	5 - 9	10 - 14	15 - 19	20 - 24	25 - 29	30 - 34	35 - 39	40 - 44	45 - 49	50 - 54	55 - 59	60				Vents		FV	NV	N	Y		
Cooling	Joy (1958)	R-7.5	Laboratory Controlled	HRB												50			N/A			S	S	X		X		Flat Roof	41%
	Katipamula & O'Neal (1986)	R-11		HRB											46				N/A			-	-	-	-	X		Flat Roof	
	Yarbrough (2010)	R-13												41					N/A			-	-	-	-	X		Pitched Roof	
	Joy (1958)	R-7.5		HRB							28								N/A			S	S	X		X		Pitched Roof	
	Swami and Fairey (1986)	R-19	Laboratory Controlled	IRCC								32							N/A			-	-	-		X		Flat Roof	32%
	Ashley et al. (1994)	R-11	Side-by-Side	HRB/TRB														60	Kingsville, TX	3,404	2	G	G		X		X	Attic fully wrapped	45%
	Medina (2000a)			TRB										42					College Station, TX	2,938	2	S	G	X		X			
	Hall (1988a)			TRB								34							Chattanooga, TN	1,608	4	S	G		X	X			
	Fairey (1985)	R-19	Side-by-Side	TRB										43					Cape Canaveral, FL	3,300	2	S	S	X		X		5 ACH, 1 AS f/down	30%
	Fairey (1985)			TRB										43					Cape Canaveral, FL	3,300	2	S	S	X		X		5 ACH, 2 AS	
	Hall (1986)			HRB										40					Chattanooga, TN	1,608	4	S	G		X	X			
	Fairey (1990)			TRB									39						Cape Canaveral, FL	3,300	2	-	-		X	X			
	Parker and Sherwin (1998)			TRB									36						Cocoa Beach, FL	3,300	2	S	R		X	X		Vent area = 1:150	
	Levins et al. (1986)			HRB									35						Karns, TN	1,301	4	S	G		X	X			
	Medina (2000a)			TRB								34							College Station, TX	2,938	2	S	G	X		X			
	Levins et al. (1986)			TRB								30							Karns, TN	1,301	4	S	G		X	X			
	Hall (1988a)			TRB								30							Chattanooga, TN	1,608	4	S	G		X	X			
	Medina et al. (1992a)			HRB								30							College Station, TX	2,938	2	S	G	X		X			
	Parker and Sherwin (1998)			TRB							26								Cocoa Beach, FL	3,300	2	S	R		X	X		Vent area = 1:300	
	Hall (1986)			TRB						23									Chattanooga, TN	1,608	4	S	G		X	X			
	McQuiston et al. (1984)			HRB						20									Stillwater, OK	1,881	3	-	-	X		-	-	Curved Roof	
	Ober & Volckhausen (1988)			DRB						20									Orlando, FL	3,428	2	S	G		X	X			
	Fairey (1985)			TRB					19										Cape Canaveral, FL	3,300	2	-	-			X		Unvented Attics	
	Fairey (1985)			HRB					18										Cape Canaveral, FL	3,300	2	-	-			X		Unvented Attics	
	Hall (1986)			DRB					16										Chattanooga, TN	1,608	4	S	G		X	X			
	Medina (2000a)	R-30	Side-by-Side	TRB							25								College Station, TX	2938	2	S	G		X	X			23%
	Hall (1988a)			TRB						20									Chattanooga, TN	1608	4	S	G		X	X			

Legend: CDD = Cooling Degree Days, HDD = Heating Degree Days, HRB = Horizontal Radiant Barrier, TRB = Truss Radiant Barrier, DARB = Deck-Applied Radiant Barrier, DRB = Draped Radiant Barrier, IRCC = Interior Radiation Control Coating, FV= Forced Ventilation, NV= Natural Ventilation, S = Soffit Vent, G = Gable Vent, R = Ridge Vent, P = Power Fan, ACH = Air Changes per Hour, AS = Aluminized Side, f/ = Facing, N/A = Not Applicable, (-) = Not Specified

Radiant barrier also showed benefits during the heating season. This is summarized in Table 2. The reductions in ceiling heat flows produced by radiant barriers, from the heated conditioned space to the attic, ranged from an average value of 13%, for attics with R-11 (1.94 m^2-K/W) insulation to 9% for attics with R-30 (5.28 m^2-K/W) insulation. For attics with R-19 (3.35 m^2-K/W) insulation the average reduction in heat flow was 12%. For attics with R-11 (1.94 m^2-K/W) insulation the HRB configuration outperformed the TRB in Zone 4, which was the only zone represented in the R-11 (1.94 m^2-K/W) pool. That is, attics with HRB had an average reduction of 18% while attics with installed TRBs reduced the heat flow by 7%. For the attics with R-19 (3.35 m^2-K/W) insulation, however, the TRB outperformed the HRB configuration, 14% to 12%, while the DRB configuration yielded an average reduction of 4%.

Table 2. Experimental Ceiling Heat Flow Reductions Produced by the RBs and IRCCs (Heating Season)

Season	Reference	Nominal Insulation Level R-Value	Testing Protocol	Method	Ceiling Heat Flow Reductions Over Test Period (%) Winter														City, St	HDD	Climatic Zone	Ventilation				Occupied		Comments	Average
					-5	0 - 4	5 - 9	10 - 14	15 - 19	20 - 24	25 - 29	30 - 34	35 - 39	40 - 44	45 - 49	50 - 54	55 - 59	60				Vents		FV	NV	N	Y		
Heating	Levins and Karnitz (1988)	R-11	Side-by-Side	HRB					19										Karns, TN	3,993	4	S	G		X	X			13%
	Hall (1988)			HRB					17										Chattanooga, TN	3,427	4	S	G		X	X			
	Levins and Karnitz (1988)			TRB			8												Karns, TN	3,993	4	S	G		X	X			
	Hall (1988)			TRB			6												Chattanooga, TN	3,427	4	S	G		X	X			
	Levins and Karnitz (1987b)	R-19	Side-by-Side	TRB								30							Karns, TN	3,993	4	S	G		X	X			12%
	Fairey (1990)			TRB						24									Cape Canaveral, FL	677	2	-	-		X	X			
	Medina et al. (1992b)			HRB					17										College Station, TX	1,616	2	-	-	-	-	X		Non-vented Attics	
	Hall (1986)			HRB					15										Chattanooga, TN	3,427	4	S	G		X	X			
	Medina et al. (1992b)			TRB					15										College Station, TX	1,616	2	-	-	-	-	X		Non-vented Attics	
	Medina et al. (1992b)			HRB				14											College Station, TX	1,616	2	S	G	X		X			
	McQuiston et al. (1984)			HRB				10											Stillwater, OK	3,989	3	-	-	X		-	-	Curved Roof	
	Medina et al. (1992b)			TRB			9												College Station, TX	1,616	2	S	G	X		X			
	Hall (1988a)			HRB			5												Chattanooga, TN	3,427	4	S	G		X	X			
	Hall (1986)			TRB			8												Chattanooga, TN	3,427	4	S	G		X	X			
	Hall (1986)			DRB		4													Chattanooga, TN	3,427	4	S	G		X	X			
	Hall (1988a)			TRB	-5														Chattanooga, TN	3,427	4	S	G		X	X			
	Hall (1988a)	R-30	Side-by-Side	HRB					15										Chattanooga, TN	3,427	4	S	G		X	X			9%
	Levins and Karnitz (1988)			HRB				10											Karns, TN	3,993	4	S	G		X	X			
	Hall (1988a)			TRB			6												Chattanooga, TN	3,427	4	S	G		X	X			
	Levins and Karnitz (1988)			TRB		4													Karns, TN	3,993	4	S	G		X	X			

Legend: CDD = Cooling Degree Days, HDD = Heating Degree Days, HRB = Horizontal Radiant Barrier, TRB = Truss Radiant Barrier, DARB = Deck-Applied Radiant Barrier, DRB = Draped Radiant Barrier, IRCC = Interior Radiation Control Coating, FV= Forced Ventilation, NV= Natural Ventilation, S = Soffit Vent, G = Gable Vent, R = Ridge Vent, P = Power Fan, ACH = Air Changes per Hour, AS = Aluminized Side, f/ = Facing, N/A = Not Applicable, (-) = Not Specified

Buildings located in Zone 2 experienced an average heat flow reduction of 16% while those located in Zone 4 experienced a reduction of 11%. The attics with installed HRBs in Zone 2 experienced an averaged reduction of 16% while those in Zones 4 and 3 experienced reductions of 10%. For those attics with R-30 (5.28 m^2-K/W) insulation, the HRB configuration produced larger reductions than the TRB configuration. The average reductions in ceiling heat flow were 13%

and 5% for the HRB and TRB configurations, respectively. All the attics with R-30 (5.28 m^2-K/W) insulation levels were also located in Zone 4. Table 3 highlights space cooling load reductions produced by the installation of radiant barriers.

Table 3. Experimental Space Cooling Load Reductions Produced by the RBs

Season	Reference	Nominal Insulation Level R-Value	Testing Protocol	Method	Ceiling Area	Space Load Reduction (%)								City, St	CDD	Climatic Zone	Ventilation				Occupied		Includes Ducts in the Attic		Average
						Cooling																			
						-5	0 - 4	5 - 9	10 - 14	15 - 19	20 - 24	25 - 29	30				Vents		FV	NV	N	Y	Y	N	
Cooling	Levins and Karnitz (1987a)	R-11	Side-by-Side	HRB	1,200					16				Karns, TN	1,301	4	S	G		X	X			X	14%
	Levins and Karnitz (1987a)			TRB	1,200				11					Karns, TN	1,301	4	S	G		X	X			X	
	Parker and Sherwin (2002)	R-19	Pre-and-Post	TRB	2,440							27		Orlando, FL	3,428	2	-	-	-	-		X		X	20%
	Levins et al. (1986)		Side-by-Side	HRB	1,200						21			Karns, TN	1,301	4	S	G		X	X			X	
	Parker and Sherwin (2002)		Pre-and-Post	TRB	2,200						20			Largo, FL	3,718	2	-	-	-	-		X	X		
	Levins et al. (1986)		Side-by-Side	TRB	1,200				13					Karns, TN	1,301	4	S	G		X	X			X	
	Parker and Sherwin (2002)	R-30	Pre-and-Post	TRB	1,520					16				Tarpon Springs, FL	3,414	2	-	-	-	-		X			6%
	Davis and Tiller (2009)		Side-by-Side	TRB	3,205				14					Charlotte, NC	1,681	3	S	R		X	X		X		
	Parker and Sherwin (2002)		Pre-and-Post	TRB	1,840			5						Apopka, FL	3,428	2	S	P	X	X		X	X		
	Levins and Karnitz (1987a)		Side-by-Side	HRB	1,200		2							Karns, TN	1,301	4	S	G		X	X			X	
	Parker and Sherwin (2002)		Pre-and-Post	TRB	2,140		0							Orlando, FL	3,428	2	P	P	X			X	Partially		
	Levins and Karnitz (1987a)		Side-by-Side	TRB	1,200	-1								Karns, TN	1,301	4	S	G		X	X			X	

Legend: CDD = Cooling Degree Days, HDD = Heating Degree Days, HRB = Horizontal Radiant Barrier, TRB = Truss Radiant Barrier, DARB = Deck-Applied Radiant Barrier, DRB = Draped Radiant Barrier, IRCC = Interior Radiation Control Coating, FV= Forced Ventilation, NV= Natural Ventilation, S = Soffit Vent, G = Gable Vent, R = Ridge Vent, P = Power Fan, ACH = Air Changes per Hour, AS = Aluminized Side, f/ = Facing, N/A = Not Applicable, (-) = Not Specified

For attics with R-11 (1.94 m^2-K/W) insulation the range of reductions in space cooling load was from 11% to 16%, with an average of 14% and for the attics with R-19 (3.35 m^2-K/W) insulation, the reductions ranged between 13% and 27%, with an average of 20%. For those houses in side-by-side testing, the average reduction in space cooling load was 17% and for the houses in pre-and-post testing the reduction was 24%. The side-by-side houses were located in Zone 4 and those in the pre-and-post were in Zone 2. The pre- and post- monitoring were one year apart and these houses were occupied, while the houses used in the side-by-side set were unoccupied. In the R-19 (3.35 m^2-K/W) insulation pool only one house had the air handling ducts in the attic. Therefore, a clear correlation as to the effects of having the ducts placed in the attic when RBs were installed could not be established. For the attics with R-30 (5.28 m^2-K/W) insulation the range of space cooling load reductions was between -1% and 16%. The "negative reduction" occurred in one of 12 cases. The average value for space cooling load reductions for attics with R-30 (5.28 m^2-K/W) insulation was 6%. Most of the houses in this pool had TRBs installed, except for one. The houses with the air handling ducts in the attics had a space cooling load reduction of 6%. Those without the ducts in the attic had an average reduction of 1%. Table 4 highlights the space heating load reductions. For attics with R-11 (1.94 m^2-K/W) insulation the average reduction in space heating load was 5%. For attics with R-19 (3.35 m^2-K/W) and R-30 (5.28 m^2-K/W) insulation the average reduction values were 4% and 4%, respectively. In each case, except for the R-30 (5.28 m^2-K/W) cluster, the HRB configuration outperformed the TRB configuration.

Table 4. Experimental Space Heating Load Reductions Produced by the RBs

Season	Reference	Nominal Insulation Level R-Value	Testing Protocol	Method	Ceiling Area	Space Load Reduction (%)								City, St	HDD	Climatic Zone	Ventilation				Occupied		Includes Ducts in the Attic		Average
						Heating																			
						-5	0 - 4	5 - 9	10 - 14	15 - 19	20 - 24	25 - 29	30				Vents		FV	NV	N	Y	Y	N	
Heating	Levins and Karnitz (1987b)	R-11	Side-by-Side	HRB	1,200			9						Karns, TN	3,993	4	S	G		X	X			X	5%
	Levins and Karnitz (1987b)			TRB	1,200		0							Karns, TN	3,993	4	S	G		X	X			X	
	Levins et al. (1986)	R-19	Side-by-Side	HRB	1,200				10					Karns, TN	3,993	4	S	G		X	X			X	4%
	Levins et al. (1986)			TRB	1,200	-3								Karns, TN	3,993	4	S	G		X	X			X	
	Levins and Karnitz (1987b)	R-30	Side-by-Side	HRB	1,200		4							Karns, TN	3,993	4	S	G		X	X			X	4%
	Levins and Karnitz (1987b)			TRB	1,200		4							Karns, TN	3,993	4	S	G		X	X			X	

Legend: CDD = Cooling Degree Days, HDD = Heating Degree Days, HRB = Horizontal Radiant Barrier, TRB = Truss Radiant Barrier, DARB = Deck-Applied Radiant Barrier, DRB = Draped Radiant Barrier, IRCC = Interior Radiation Control Coating, FV= Forced Ventilation, NV= Natural Ventilation, S = Soffit Vent, G = Gable Vent, R = Ridge Vent, P = Power Fan, ACH = Air Changes per Hour, AS = Aluminized Side, f/ = Facing, N/A = Not Applicable, (-) = Not Specified

Table 5 highlights the reductions in attic temperature produced by the radiant barriers. Attics in which TRBs were installed showed temperature reductions from 3°F to 23°F (1.7°C to 12.8°C). When the attics had R-11 (1.94 m^2-K/W) insulation the average temperature reduction was 9°F (5°C). In attics with R-19 (3.35 m^2-K/W) insulation the average temperature reduction was 14°F (7.8°C). It was 11 °F (6.1°C) for attics with R-30 (5.28 m^2-K/W) insulation. For attics with R-19 (3.35 m^2-K/W) insulation, those located in Zone 2 and Zone 4 had average temperature reductions of 14°F (7.8°C) and 13°F (7.2°C), respectively. Two attics in the R-19 (3.35 m^2-K/W) insulation pool had HRBs installed and both were located in Zone 4. In one house the temperature reduction after the installation of an HRB was 8°F (4.4°C) while in the other it was

0°F (0°C). Because of the manner in which sensors (e.g., thermocouples) may have been installed in the attics and the way data were collected and reported, the above temperature reductions represent a mix of attic air temperature reductions and top of insulation temperature reductions.

Table 5. Experimental Attic Temperature Reductions Produced by the RBs (Cooling Season)

Season	Reference	Nominal Insulation Level R-Value	Testing Protocol	Method	Temperature Reductions (Deg F)														City, St	CDD	Climatic Zone	Ventilation				Occupied		Comments	Average
					Summer																								
					0	0 - 2	3 - 4	5 - 6	7 - 8	9 - 10	11 - 12	13 - 14	15 - 16	17 - 18	19 - 20	21 - 22	23 - 24	25 - 26				Vents		FV	NV	N	Y		
Cooling	Hall (1988a)	R-11	Side-by-Side	TRB						10									Chattanooga, TN	1,608	4	S	G		X	X			9 F
	Levins and Karnitz (1987a)								7										Karns, TN	1,301	4	S	G		X	X			
	Parker and Sherwin (1998)	R-19	Side-by-Side	TRB											20				Cocoa Beach, FL	3,300	2	S	R		X	X		Vent area = 1:150	14 F
	Parker and Sherwin (2002)		Pre-and-Post										16						Orlando, FL	3,428	2	-	-	-	-		X		
	Parker and Sherwin (2002)		Pre-and-Post										15						Largo, FL	3,718	2	-	-	-	-		X		
	Levins and Karnitz (1986)		Side-by-Side										15						Karns, TN	1,301	4	S	G		X	X			
	Hall (1988a)		Side-by-Side							10									Chattanooga, TN	1,608	4	S	G		X	X			
	Parker and Sherwin (1998)		Side-by-Side					6											Cocoa Beach, FL	3,300	2	S	R		X	X		Vent area = 1:300	
	Hall (1986)		Side-by-Side	HRB					8										Chattanooga, TN	1,608	4	S	G		X	X			4 F
	Levins and Karnitz (1986)		Side-by-Side			0													Karns, TN	1,301	4	S	G		X	X			
	Davis and Tiller (2009)	R-30	Side-by-Side	TRB												23			Charlotte, NC	1,681	3	S	R		X				11 F
	Parker and Sherwin (2002)		Pre-and-Post													22			Tarpon Springs, FL	3,414	2	-	-	-	-		X		
	Parker and Sherwin (2002)		Pre-and-Post								11								Apopka, FL	3,428	2	S	P	X	X		X		
	Hall (1988a)		Side-by-Side							10									Chattanooga, TN	1,608	4	S	G		X	X			
	Levins and Karnitz (1987a)		Side-by-Side						7										Karns, TN	1,301	4	S	G		X	X			
	Parker and Sherwin (2002)		Pre-and-Post				3												Orlando, FL	3,428	2	P	P	X			X		

Legend: CDD = Cooling Degree Days, HDD = Heating Degree Days, HRB = Horizontal Radiant Barrier, TRB = Truss Radiant Barrier, DARB = Deck-Applied Radiant Barrier, DRB = Draped Radiant Barrier, IRCC = Interior Radiation Control Coating, FV= Forced Ventilation, NV= Natural Ventilation, S = Soffit Vent, G = Gable Vent, R = Ridge Vent, P = Power Fan, ACH = Air Changes per Hour, AS = Aluminized Side, f/ = Facing, N/A = Not Applicable, (-) = Not Specified

Table 6. Simulated Results Highlighting Space Cooling Load Reductions Produced by Interior Radiation Control Coatings

(CONTINUED) SIMULATED RESULTS HIGHLIGHTING SPACE COOLING LOAD REDUCTIONS PRODUCED BY THE RADIANT BARRIERS AND INTERIOR RADIATION CONTROL COATINGS

Season	Reference	Nominal Insulation Level R-Value	Model	Method	Ceiling Area	Cooling Load Base (kWh)	Cooling Load w/RB (kWh)	Space Load Reduction (%)								City, St	CDD	Climatic Zone	Ventilation				Includes Ducts in the Attic		Duct Insulation Level	Duct Leakage Rate		Average
								Cooling																				
								-5	0 - 4	5 - 9	10 - 14	15 - 19	20 - 24	25 - 29	30->				Vents		FV	NV	Y	N		Supply	Return	
Cooling	Enercomp (2008)	R-11	Micropas	IRCC (E = 0.20)	1,500	101	69								32	CA Climatic Zone 1	-	3	-	-		1/300	X		R-4.2	Duct Leakage Factor = 0.89		14%
						3,931	3,457				12					CA Climatic Zone 2	-	3										
						697	563					19				CA Climatic Zone 3	-	3										
						2,555	2,195				14					CA Climatic Zone 4	-	3										
						820	648						21			CA Climatic Zone 5	-	3										
						1,099	905					18				CA Climatic Zone 6	-	3										
						1,849	1,543					17				CA Climatic Zone 7	-	3										
						3,953	3,430				13					CA Climatic Zone 8	-	3										
						5,483	4,854				11					CA Climatic Zone 9	-	3										
						7,382	6,623				10					CA Climatic Zone 10	-	4										
						7,691	7,008			9						CA Climatic Zone 11	-	3										
						5,962	5,410			9						CA Climatic Zone 12	-	3										
						10,790	9,842			9						CA Climatic Zone 13	-	3										
						9,086	8,355			8						CA Climatic Zone 14	-	4										
						19,593	18,312			7						CA Climatic Zone 15	-	5										
						2,530	2,202				13					CA Climatic Zone 16	-	2										

Legend: CDD = Cooling Degree Days, HDD = Heating Degree Days, HRB = Horizontal Radiant Barrier, TRB = Truss Radiant Barrier, DARB = Deck-Applied Radiant Barrier, DRB = Draped Radiant Barrier, IRCC = Interior Radiation Control Coating, FV= Forced Ventilation, NV= Natural Ventilation, S = Soffit Vent, G = Gable Vent, R = Ridge Vent, P = Power Fan, ACH = Air Changes per Hour, AS = Aluminized Side, f/ = Facing, N/A = Not Applicable, (-) = Not Specified

CONCLUSIONS

There is ample evidence in the literature to conclude that Radiant Barriers and Interior Radiation Control Coatings reduce the heat transfer rate across attic spaces in a significant manner. This reduction translated into considerable reductions in space cooling and to a lesser extent in space heating loads. The reductions in ceiling heat flow were primarily affected by RB and IRCC's emittance values, the level of insulation in the attic, and climate. The data indicated that, on average, radiant barriers reduced summer ceiling heat flows by approximately 23 to 45% depending on the insulation level. Winter ceiling heat flow reductions were approximately 40% of the summer values for the same insulation levels. The data also indicated that space cooling loads were reduced between 6 to 20% with space heating load reductions being also about 40% of cooling values for the same insulation levels. Data from laboratory controlled experiments indicated that IRCCs with an emittance of 0.25 or less would provide reductions equivalent to 61% of the values produced by the radiant barriers. The data also indicated that DARBs and TRBs would reduce the summer attic air temperature by an average of 13°F (7.2 °C) and would increase shingle temperature by an average of 5°F (2.8°C). Radiant barriers installed in the HRB configuration would reduce the attic air temperature by an average of 4°F (2.2 °C) and increase the shingle temperature by 1 °F (0.6 °C).

NOMENCLATURE

A = surface area, ft^2 or m^2
ε = emittance of surface 1 or surface 2
F = configuration factor (a function only of geometry)
q = ceiling heat flux, Btu/hr-ft^2 or W/m^2
σ = Stefan-Boltzmann constant, 0.1713 x 10^{-8} Btu/(hr-ft^2-R^4) = 5.673 x 10^{-8} W/(m^2-K^4)
T = absolute temperature, R or K

REFERENCES

ASHRAE. 2006. *ASHRAE Standard* 169-2006. *Weather Data for Building Design Standards*. Atlanta: American Society of Heating, Refrigerating, and Air Conditioning Engineers, Inc.

Ashley, R., Garcia, O., Medina, M.A., and Turner, W.D. 1994. Effects of radiant barrier technology on summer attic heat load in South Texas. *Proceedings of the 9th Symposium on Improving Building Systems in Hot and Humid Climates*, Arlington, TX.

ASTM C1313. 2010. *Standard Specification for Sheet Radiant Barriers for Building Construction Applications*. Philadelphia: American Society for Testing Materials.

ASTM C1321. 2009. *Standard Practice for Installation and Use of Interior Radiation Control Coating Systems (IRCCS) in Building Construction*. Philadelphia: American Society for Testing Materials.

Carter, T. 2010. Attic insulation - blown vs. batt. www.askthebuilder.com/165__Attic_Insulation_-_Blown_vs_Batt.shtml.

Davis, B. and Tiller, J. 2009. Radiant barrier impact on selected building performance measurements - Model home case study. Energy Center, Appalachian State University, USA.

Fairey P.W. 1985. The measured side-by-side performance of attic radiant barrier systems in hot, humid climates. *Proceedings of the 19th International Thermal Conductivity Conference*, Cookeville, TN.

Fairey P.W. 1990. Seasonal prediction of roof-mounted attic radiant barrier system performance from measured test data. *Proceedings of the ACEEE 1990 Summer Study on Energy Efficiency in Buildings*, Pacific Grove, CA.

Hall, J. A. 1986. Performance testing of radiant barriers. *Proceedings of the 3rd Symposium on Improving Building Systems in Hot and Humid Climates*, Arlington, TX.

Hall J. A. 1988. Radiant barrier testing to assess effects of dust accumulation, attic ventilation, and other key variables. Report TVA/OP/EDT-88/25, Tennessee Valley Authority, U.S.A.

Hall, J. A. 1988a. Performance testing of radiant barriers (RB) with R-11, R-19, and R-30 cellulose and rock wool insulation. *Proceedings of the 5th Symposium on Improving Building Energy Efficiency in Hot and Humid Climates*, Houston, TX.

Joy F.A. 1958. Improving attic space insulating values. *ASHRAE Transaction* Vol. 64: 251-266.

Katipamula S. and O'Neal D.L. 1986. An evaluation of the placement of radiant barriers on their effectiveness in reducing heat transfer in attics. *Proceedings of the 3rd Symposium on Improving Building Energy Efficiency in Hot and Humid Climates*, Arlington, TX.

Lenntech. 2010. Aluminum. www.lenntech.com/periodic/elements/al.htm.

Levins W.P. and Karnitz M.A. 1986. Cooling energy measurements of unoccupied single-family houses with attics containing radiant barriers. Report ORNL/CON-200, Oak Ridge National Laboratory, U.S.A.

Levins W.P., Karnitz M.A., and Knight D.K. 1986. Cooling energy measurements of unoccupied single-family houses with attics containing radiant barriers. *Proceedings of the 3rd Symposium on Improving Building Energy Efficiency in Hot and Humid Climates*, Arlington, TX.

Levins W.P. and Karnitz M.A. 1987a. Cooling energy measurements of single-family houses with attics containing radiant barriers in combination with R-11 and R-30 ceiling insulation. Report ORNL/CON-226, Oak Ridge National Laboratory. U.S.A.

Levins W.P. and Karnitz M.A. 1987b. Heating energy measurements of unoccupied single-family houses with attics containing radiant barriers. Report ORNL/CON-213, Oak Ridge National Laboratory. U.S.A.

Levins W.P. and Karnitz M.A. 1988. Heating energy measurements of single-family houses with attics containing radiant barriers in combination with R-11 and R-30 ceiling insulation. Report ORNL/CON-239, Oak Ridge National Laboratory. U.S.A.

McQuiston, F.C., Der, S.L., and Sandoval, S.B. 1984. Thermal simulation of attic and ceiling spaces. *ASHRAE Transactions*, Vol. 90, Pt 1, pp. 139-163.

Medina, M.A., O'Neal, D.L., and Turner, W.D. 1992a. Effect of attic ventilation on the performance of radiant barriers. *ASME Journal of Solar Energy Engineering*, Vol. 114, pp. 234 - 239.

Medina, M.A., O'Neal, D.L., and Turner, W.D. 1992b. Radiant barrier performance during the heating season. *Proceedings of the 8th Symposium on Improving Building Energy Efficiency in Hot and Humid Climates,* Dallas, TX.

Medina, M.A. 2000a. Radiant Barriers: Performance Revealed," *Home Energy Magazine,* September/October issue.

Ober D.G. and Volckhausen T.W. 1988. Radiant barrier insulation performance in full-scale attics with soffit and ridge venting. *Proceedings of the 5th Symposium on Improving Building Energy Efficiency in Hot and Humid Climates*, Houston, TX.

Parker, D. and Sherwin, J. 1998. Comparative summer attic thermal performance of six roof constructions. *Proceedings of the 1998 ASHRAE Annual Meeting*, Toronto, Canada.

Parker, D. and Sherwin, J. 2002. Influence of attic radiant barrier systems on air conditioning demand in an utility pilot project. *Proceedings of the 13th Symposium on Improving Building Systems in Hot and Humid Climates*, Houston, TX.

Swami, M.V., and Fairey, P. 1986. Comparative testing of a low emissivity paint. Report FSEC-CR-155-86, Florida Solar Energy Center, U.S.A.

Yarbrough, D. W. 2010. Measured thermal performance for horizontal radiant barriers installed above attic floor insulation. Report RD10216, R&D Services, U.S.A.